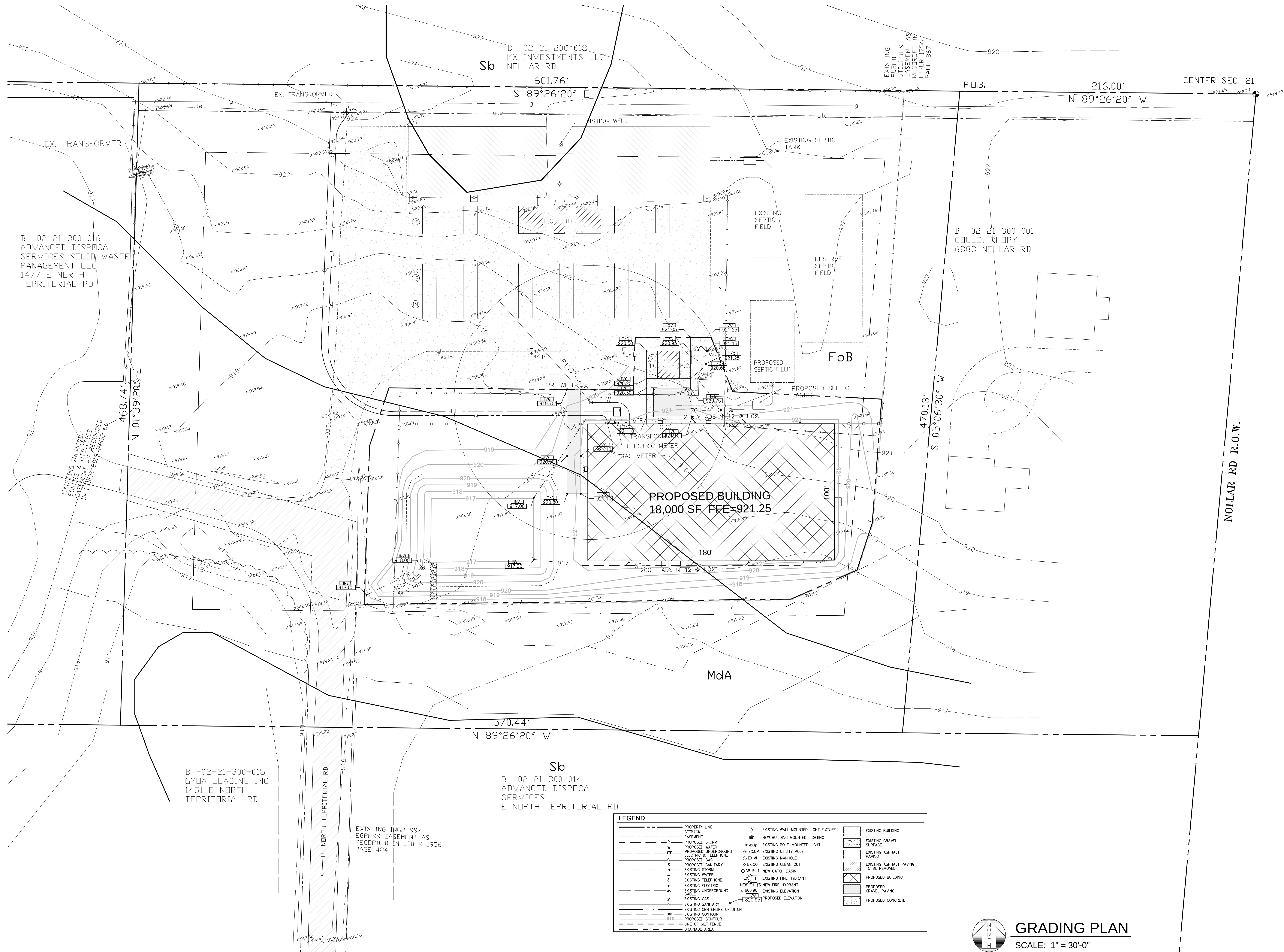
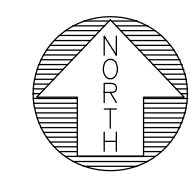




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| LEGEND |                                           |  |                                     |  |                                       |
|--------|-------------------------------------------|--|-------------------------------------|--|---------------------------------------|
|        | PROPERTY LINE                             |  | EXISTING WALL MOUNTED LIGHT FIXTURE |  | EXISTING BUILDING                     |
|        | SETRACK EASEMENT                          |  | NEW BUILDING MOUNTED LIGHTING       |  | EXISTING GRAVEL SURFACE               |
|        | PROPOSED STORM                            |  | EXISTING POLE-MOUNTED LIGHT         |  | EXISTING ASPHALT PAVING               |
|        | PROPOSED WATER                            |  | EXISTING UTILITY POLE               |  | EXISTING ASPHALT PAVING TO BE REMOVED |
|        | PROPOSED UNDERGROUND ELECTRIC & TELEPHONE |  | EXISTING MANHOLE                    |  | PROPOSED BUILDING                     |
|        | PROPOSED GAS                              |  | EXISTING CLEAN OUT                  |  | PROPOSED GRAVEL PAVING                |
|        | PROPOSED SANITARY                         |  | NEW CATCH BASIN                     |  | PROPOSED CONCRETE                     |
|        | EXISTING STORM                            |  | EXISTING FIRE HYDRANT               |  |                                       |
|        | EXISTING WATER                            |  | NEW FIRE HYDRANT                    |  |                                       |
|        | EXISTING TELEPHONE                        |  | EXISTING ELEVATION                  |  |                                       |
|        | EXISTING ELECTRIC                         |  | PROPOSED ELEVATION                  |  |                                       |
|        | EXISTING UNDERGROUND CABLE                |  |                                     |  |                                       |
|        | EXISTING GAS                              |  |                                     |  |                                       |
|        | EXISTING SANITARY                         |  |                                     |  |                                       |
|        | EXISTING CENTERLINE OF DITCH              |  |                                     |  |                                       |
|        | EXISTING CONTOUR                          |  |                                     |  |                                       |
|        | PROPOSED CONTOUR                          |  |                                     |  |                                       |
|        | LINE OF SILT FENCE                        |  |                                     |  |                                       |
|        | DRAINAGE AREA                             |  |                                     |  |                                       |



**GRADING PLAN**  
SCALE: 1" = 30'-0"

ANN ARBOR DOG TRAINING

DESIGNERS  
**Vanston/O'Brien, Inc.**  
BUILDERS

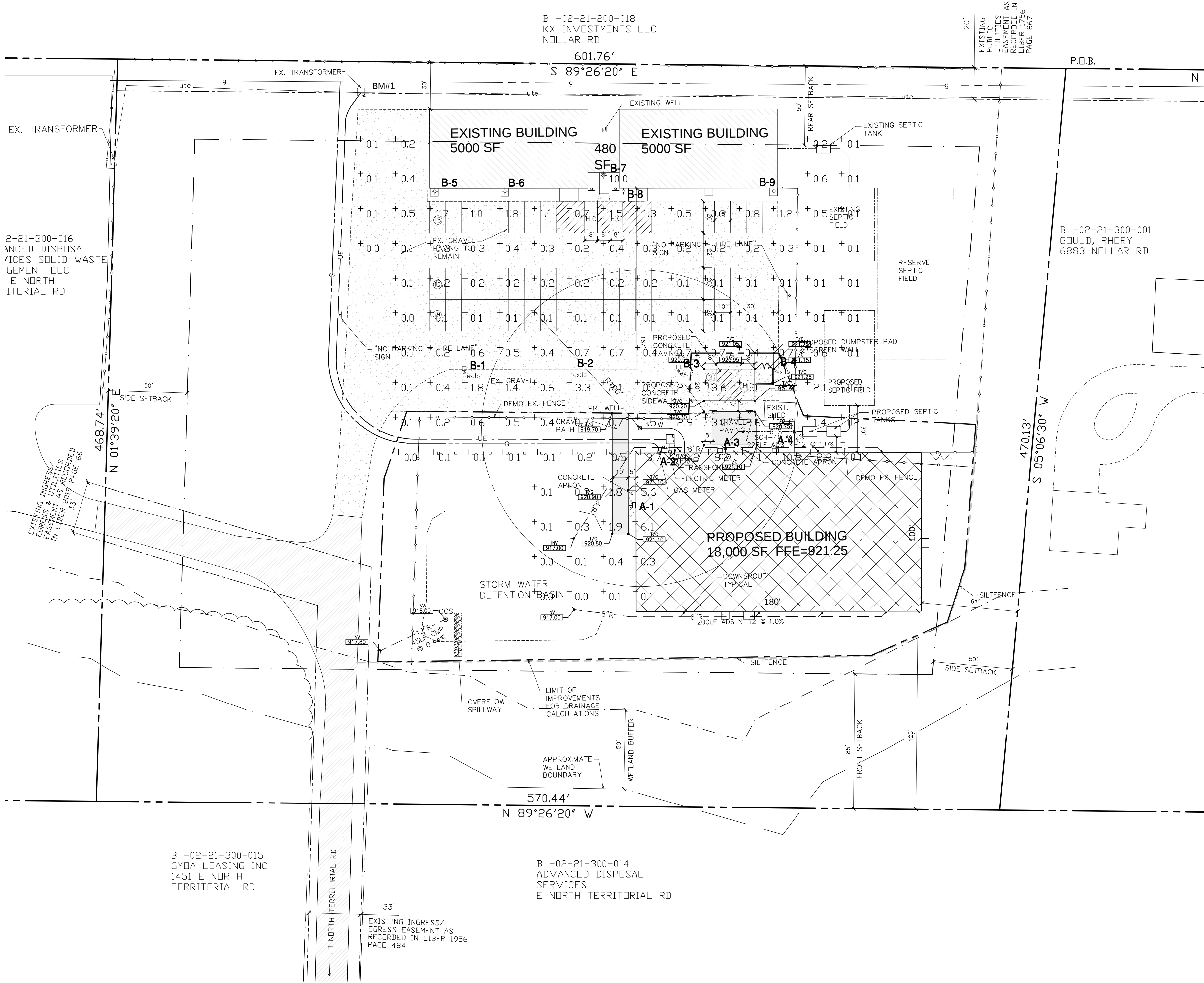
2375 Bishop Circle West  
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|                 |        |
|-----------------|--------|
| ISSUED FOR:     | DATE:  |
| CONDITIONAL USE | 3-9-17 |
| SITE PLAN       | 5-9-17 |
| REVISED         | 6-5-17 |

DRAWN BY: GAH/CLN  
JOB NO.:

**GRADING PLAN**  
SHEET NO.  
**C-2**



 **LIGHTING PLAN**  
SCALE: 1" = 40'-0"

**Arrangement**

Single  
Arm : 0 ft  
Offset : -- ft

**Layout**

Cols (X) Rows (Y)  
Layout : Varies Varies  
Spacing : Varies Varies ft  
Mounting Height : 16 ft  
Orient : Varies deg  
Tilt : 0 deg

**Statistical Analysis**

**Illuminance Values**  
Average : 1.14 fc  
Maximum : 14.98 fc  
Minimum : 0.00 fc  
Avg/Min Ratio : N.A. fc  
Max/Min Ratio : N.A. fc  
Max/Avg Ratio : 13.17 fc

**Arrangement**

Single  
Arm : 1 ft  
Offset : -- ft

**Layout**

Cols (X) Rows (Y)  
Layout : Varies Varies  
Spacing : Varies Varies ft  
Mounting Height : 16 ft  
Orient : 90 deg  
Tilt : 0 deg

**Statistical Analysis**

**Illuminance Values**  
Average : 0.55 fc  
Maximum : 5.69 fc  
Minimum : 0.02 fc  
Avg/Min Ratio : 26.98 fc  
Max/Min Ratio : 280.63 fc  
Max/Avg Ratio : 10.40 fc

**Arrangement**

Single  
Arm : 1 ft  
Offset : -- ft

**Layout**

Cols (X) Rows (Y)  
Layout : Varies Varies  
Spacing : Varies Varies ft  
Mounting Height : Varies ft  
Orient : 270 deg  
Tilt : 0 deg

**Statistical Analysis**

**Illuminance Values**  
Average : 0.67 fc  
Maximum : 10.83 fc  
Minimum : 0.01 fc  
Avg/Min Ratio : 45.63 fc  
Max/Min Ratio : 741.66 fc  
Max/Avg Ratio : 16.25 fc



**Luminaire Location Summary**

| N | Arrangement | Lum # | X     | Y     | Z    | Orient | Tilt | Tilt Factor |
|---|-------------|-------|-------|-------|------|--------|------|-------------|
| 1 | Single      | A     | -44.2 | -33.0 | 16.0 | 180    | 0    | 1.000       |
| 2 | Single      | A     | -26.0 | 0.0   | 16.0 | 90     | 0    | 1.000       |
| 3 | Single      | A     | 9.0   | 0.0   | 16.0 | 90     | 0    | 1.000       |
| 4 | Single      | A     | 44.3  | 0.0   | 16.0 | 90     | 0    | 1.000       |



**Luminaire Location Summary**

| N | Arrangement | Lum # | X      | Y   | Z    | Orient | Tilt | Tilt Factor |
|---|-------------|-------|--------|-----|------|--------|------|-------------|
| 1 | Single      | B     | -101.0 | 0.0 | 16.0 | 90     | 0    | 1.000       |
| 2 | Single      | B     | -34.0  | 0.0 | 16.0 | 90     | 0    | 1.000       |
| 3 | Single      | B     | -34.0  | 1.0 | 16.0 | 90     | 0    | 1.000       |
| 4 | Single      | B     | 95.4   | 0.0 | 16.0 | 90     | 0    | 1.000       |



**Luminaire Location Summary**

| N | Arrangement | Lum # | X      | Y    | Z    | Orient | Tilt | Tilt Factor |
|---|-------------|-------|--------|------|------|--------|------|-------------|
| 5 | Single      | B     | -107.0 | -5.0 | 16.0 | 270    | 0    | 1.000       |
| 6 | Single      | B     | -62.5  | -6.0 | 16.0 | 270    | 0    | 1.000       |
| 7 | Single      | B     | 0.0    | -5.0 | 12.0 | 270    | 0    | 1.000       |
| 8 | Single      | B     | 12.5   | -5.0 | 16.0 | 270    | 0    | 1.000       |
| 9 | Single      | B     | 107.0  | -5.0 | 16.0 | 270    | 0    | 1.000       |



**Luminaire A Proposed**

IES Filename : E-AL3L315NZ.IES  
Description : E-AL3L315NZ  
LED wall pack. Black metal housing with integrated heat sink.  
Two Cree CXA3050 LED arrays

Light Loss Factor : 0.72  
Number of Lamps : 1  
Lamp Lumens : ~1 lms  
Luminaire Watts : 151 W



**Luminaire B Existing**

IES Filename : E-DD1L68C1.IES  
Description : E-DD1L68C1  
Gray painted metal fixture with one mounting arm on the back. One LED array.  
One type CXX array

Light Loss Factor : 0.72  
Number of Lamps : 1  
Lamp Lumens : ~1 lms  
Luminaire Watts : 66 W



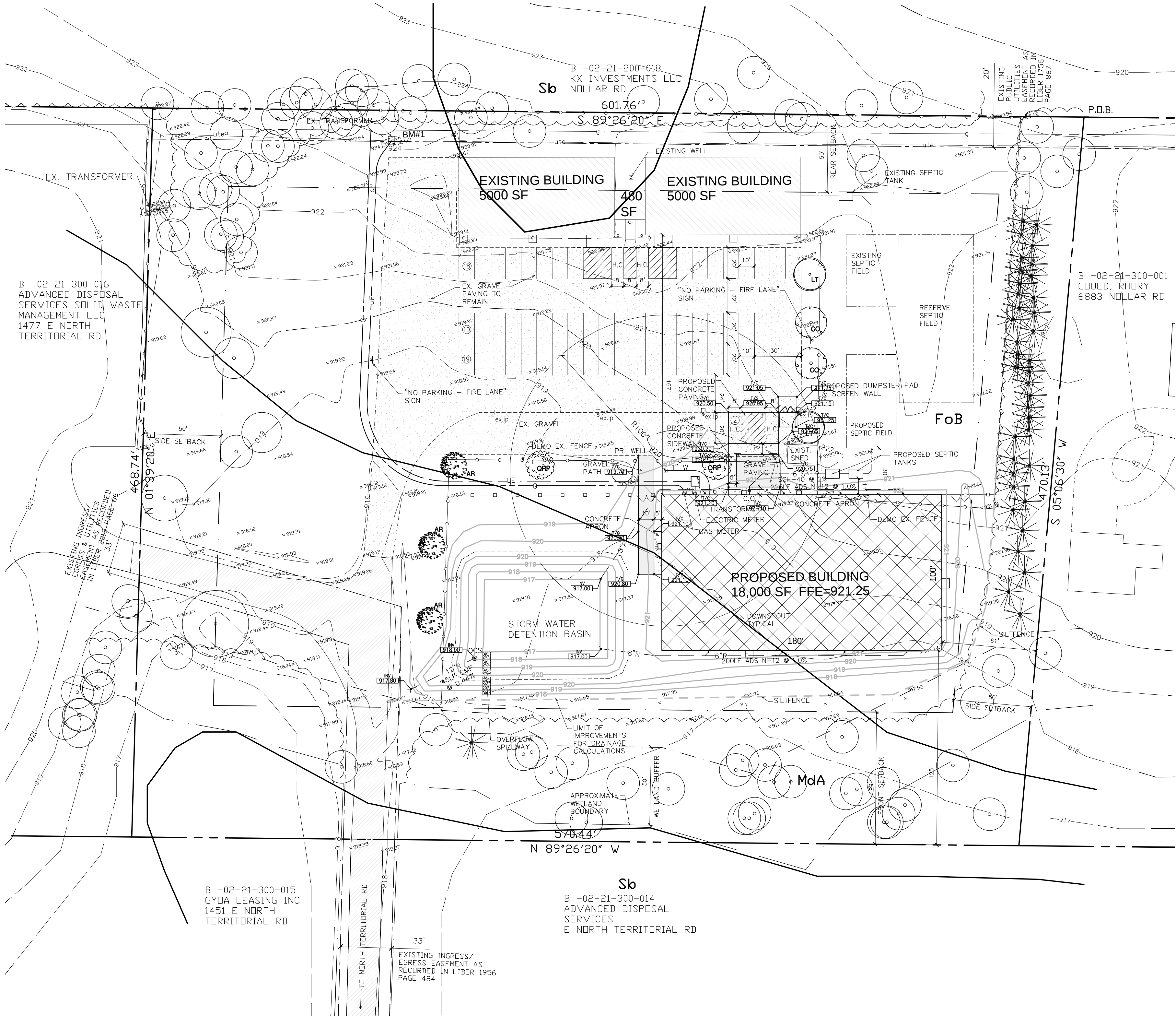
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1575 E. North Territorial Road  
Northfield Township, Michigan

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SITE PLAN 5-9-17  
REVISED 6-5-17

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JOB NO.: ---

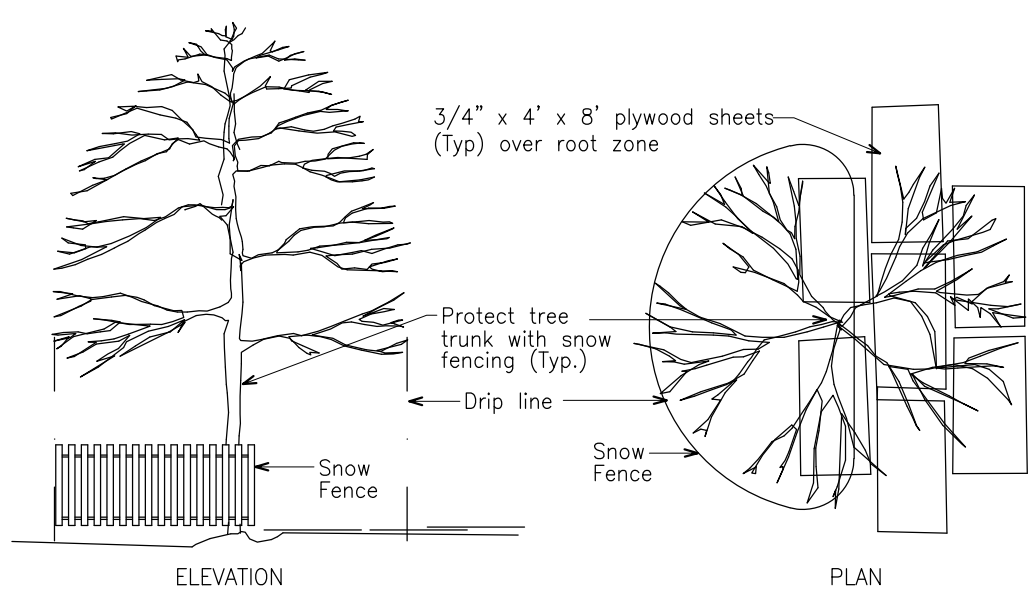
LIGHTING PLAN  
SHEET NO.

C-3



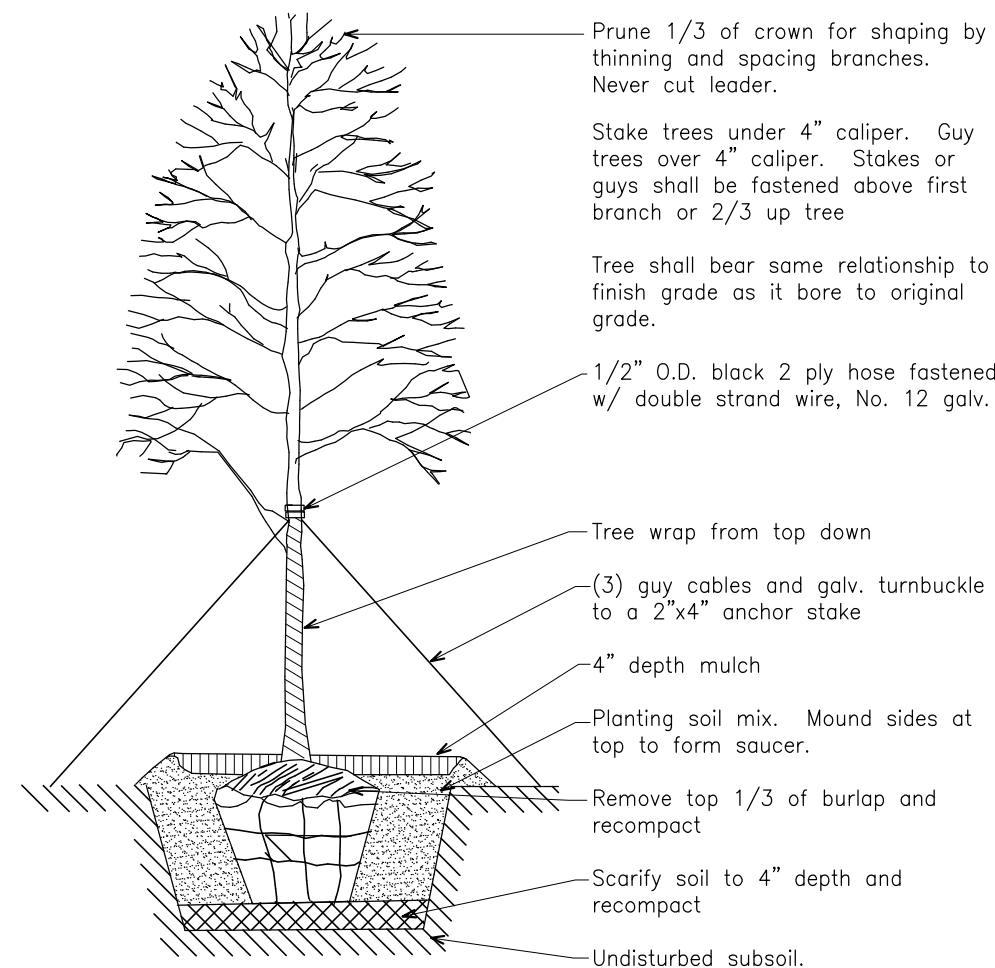
LANDSCAPE PLAN

SCALE: 1" = 40'-0"



STANDARD TREE PROTECTION

NOTE: Pull back fencing to install plywood when access in root zone is necessary.



DECIDUOUS TREE PLANTING DETAIL

Landscape Notes

- All plant material shall meet current American Association of Nurserymen, Inc. (AAN) standard for nursery stock. (ANSI 260.1 - 1973)
- Landscape installation shall be in accordance with the American Association of Nursery standards and with the Township/City's landscape requirements.
- Planting schedules: 1) Deciduous material shall be planted from March 15 for spring planting and from October 1 until the ground freezes for fall planting. 2) Evergreen material shall be planted from March 1 through May 31 for Spring plantings and from August 1 through September 30 for all fall planting.
- Mulch plant beds, individual tree and shrub planting pits uniform depth of 4 inches.
- Provide weed mat for greenbelt and foundation plantings.
- All planting beds are to be edged. Recommended either "Permaloc Aluminum" edging or "Black Diamond" plastic edging.
- All areas with stone cover shall have weed mat.
- All landscaping to be continuously maintained.
- All site improvements detailed on this plan are to be completed prior to issuance of final certificate of occupancy.
- All construction to conform to the latest applicable Township/City regulations.
- R.O.W. areas to be seeded or sod.
- Tree protection consists of:
  - Yellow ribbon barriers for large areas not disturbed by construction.
  - Stakes 10' on center and wood snow fence around individual and groups of individual trees.
  - Trees to be removed will be tagged with red ribbon.
- The barrier or fence surrounding the tree or group of trees shall be located no closer to the tree than the tree's drip line. If this is not possible, the barrier shall be no closer than 6 feet from the trunk of the tree or group of trees.
- There will be no outside storage on site.
- Seed Mix
  - Temporary planting mixture for erosion control.
    - Seed Oats 30 pounds per acre
    - Annual Rye 10 pounds per acre
  - Permanent planting mixture on all disturbed areas, excluding BMPs.
    - Scalds Hard Fescue 12 pounds per acre
    - Danson's Creeping Red Fescue 6 pounds per acre
    - Perennial Rye 20 pounds per acre
    - Buffalo Grass 20 pounds per acre
    - Creeping Bent 0.5 pounds per acre
    - Little Blue Stem 20 pounds per acre
    - Sheep Fescue 15 pounds per acre
- Rain Water Garden / Infiltration Basin Plantings
  - Within areas above the first flush elevation of the infiltration basins, seeding and/or live plantings are allowed. Only native seeds (as defined by Michigan Flora, [www.michiganflora.net](http://www.michiganflora.net)) are allowed for permanent soil stabilization. Annual seeds are allowed in an amount necessary to temporarily stabilize the limits of disturbance.
  - Within areas below the first flush elevation of the infiltration basins, only live plantings are allowed in a storm water system of any kind. Native plants are preferred. Cultivars and non-native perennials are allowable if approved by WCWRC. Plants listed on the WCWRC Rain Garden Plant List are acceptable. Invasive species are not allowed (see the City of Ann Arbor's invasive species list).
- Large trees shall not be planted directly on top of utility pipes or service leads.

PLANT LIST

TREES

| KEY | QTY | SPECIES                    | SIZE     | SPECS |
|-----|-----|----------------------------|----------|-------|
| AR  | 3   | Acer rubrum 'Autumn Blaze' | 2.5" cal | B&B   |
| CO  | 2   | Autumn Blaze Red Maple     | 2.5" cal | B&B   |
| LT  | 2   | Celtis occidentalis        | 2.5" cal | B&B   |
| QRP | 2   | Hackberry                  | 2.5" cal | B&B   |
|     | 2   | Liriodendron tulipifera    | 2.5" cal | B&B   |
|     | 2   | Tulip Poplar               | 2.5" cal | B&B   |
|     | 2   | Quercus x warei 'Long'     | 2.5" cal | B&B   |
|     | 2   | Regal Prince Oak           | 2.5" cal | B&B   |



DESIGNERS  
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**ANN ARBOR DOG TRAINING**  
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**Northfield Township, Michigan**

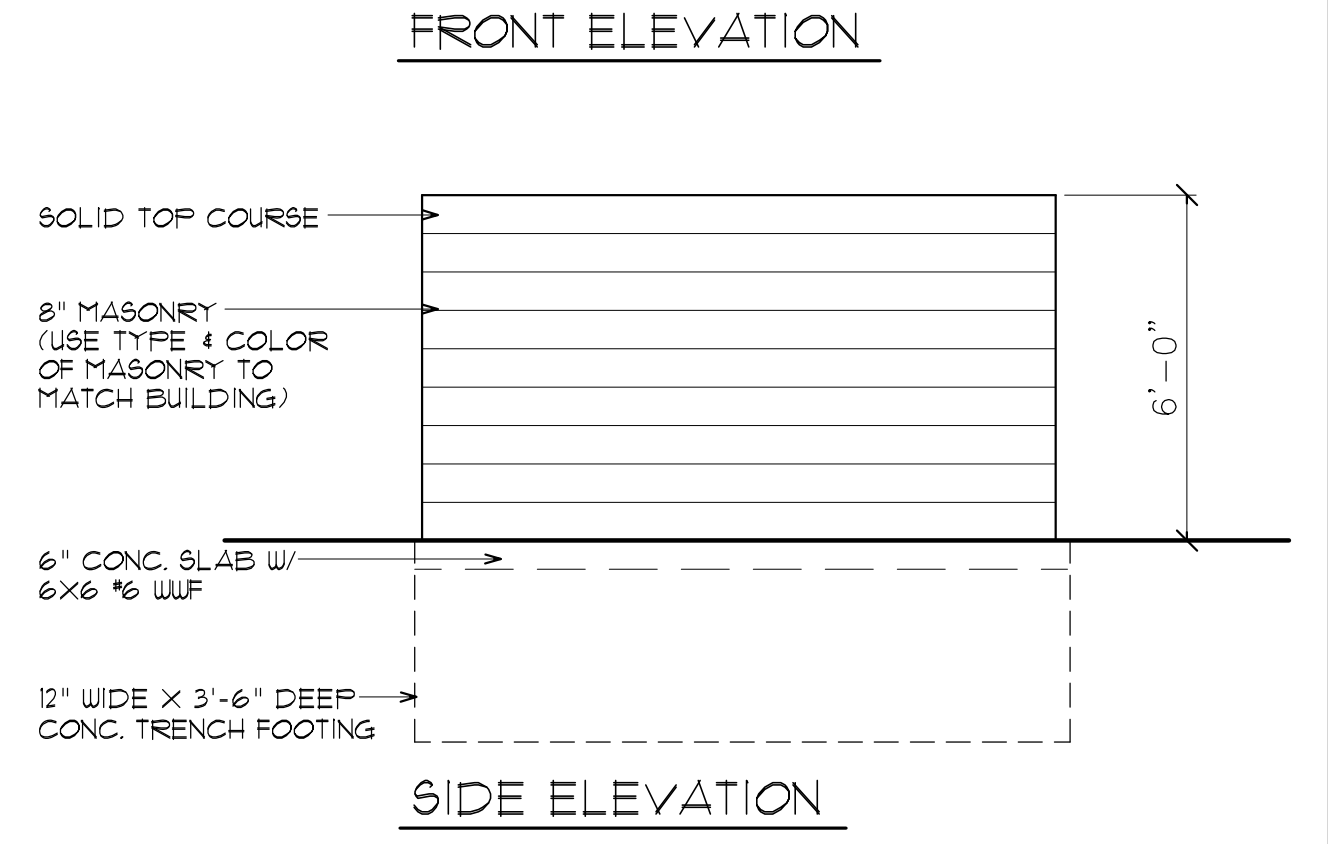
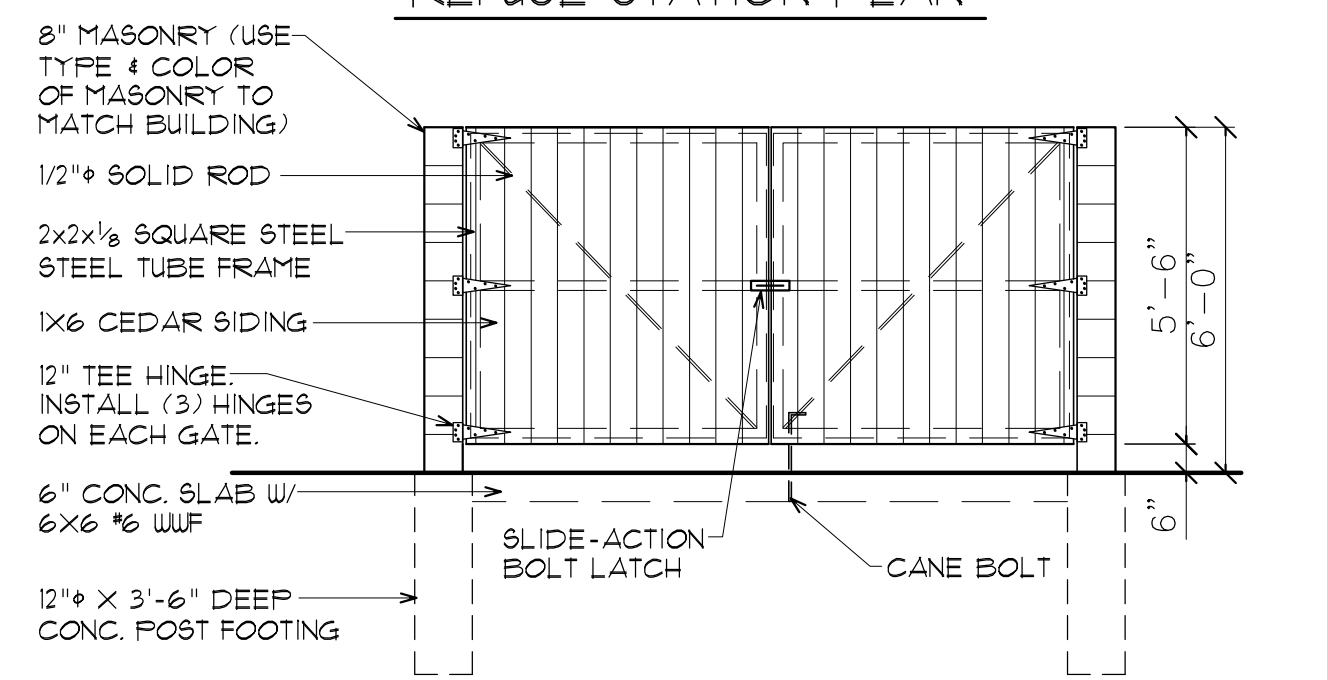
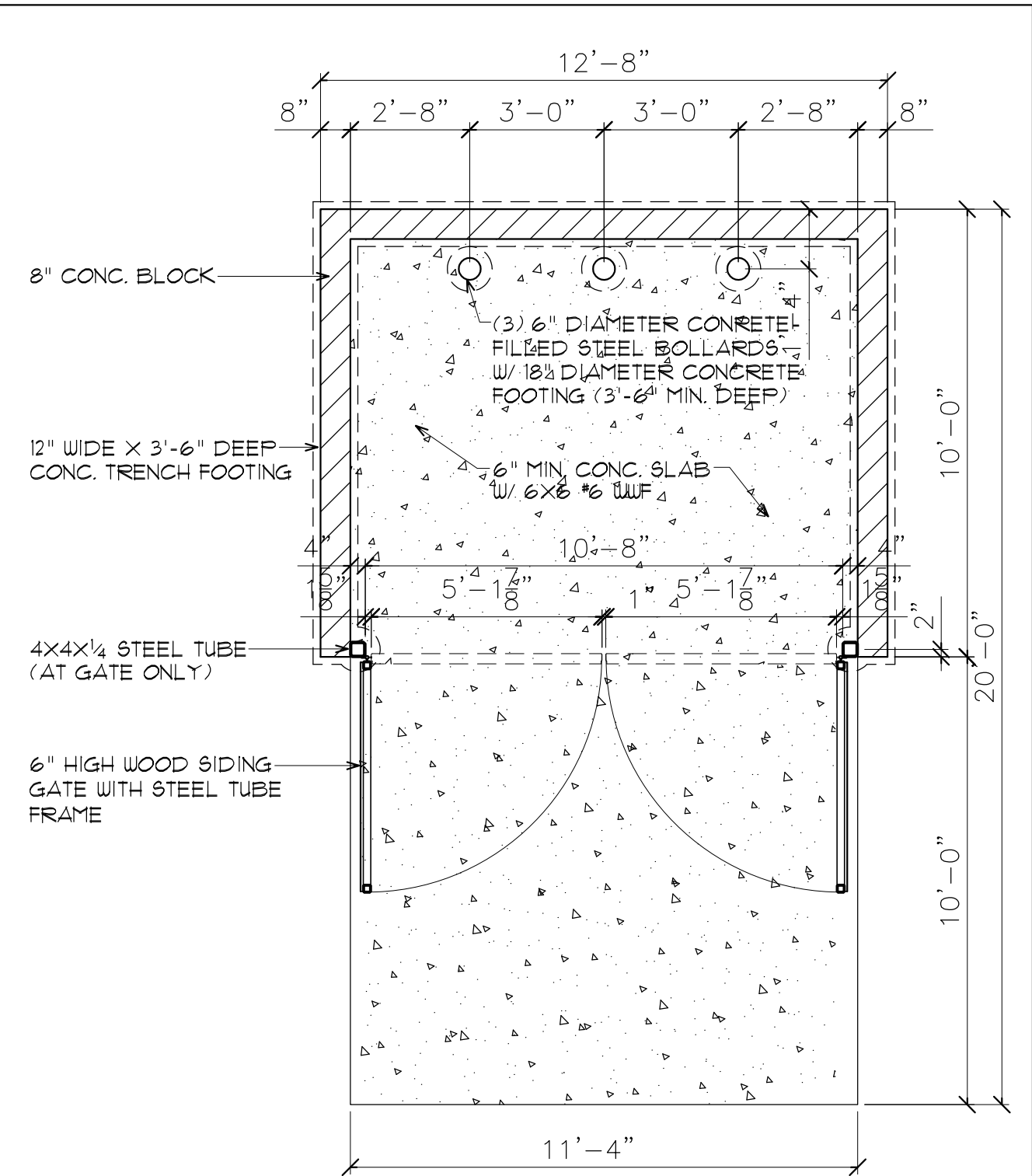
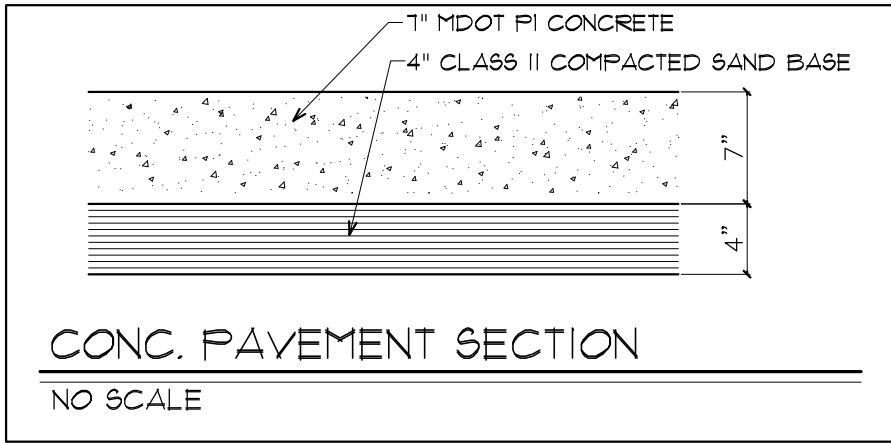
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ISSUED FOR: DATE:  
CONDITIONAL USE 3-9-17  
SITE PLAN 5-9-17  
REVISED 6-5-17

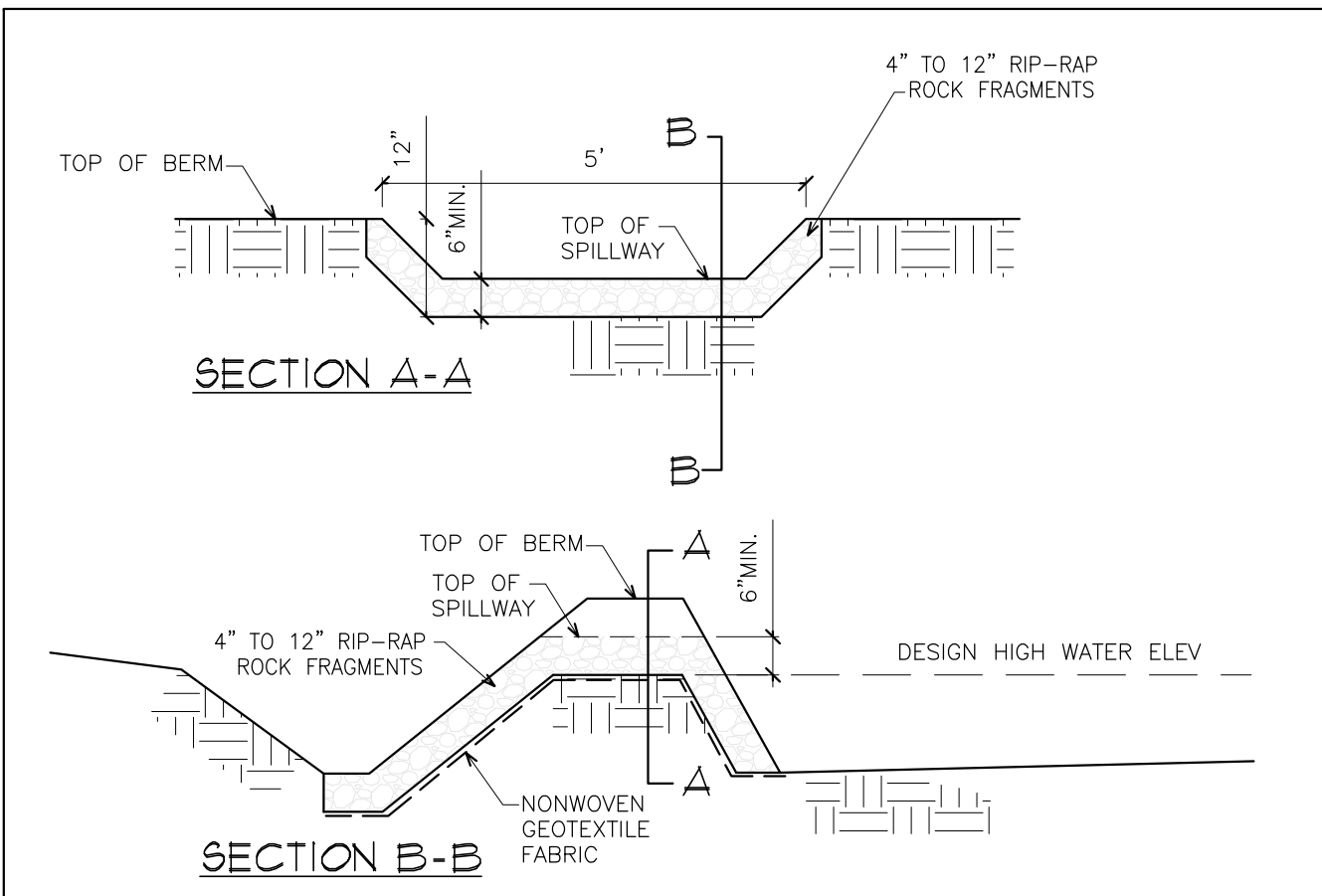
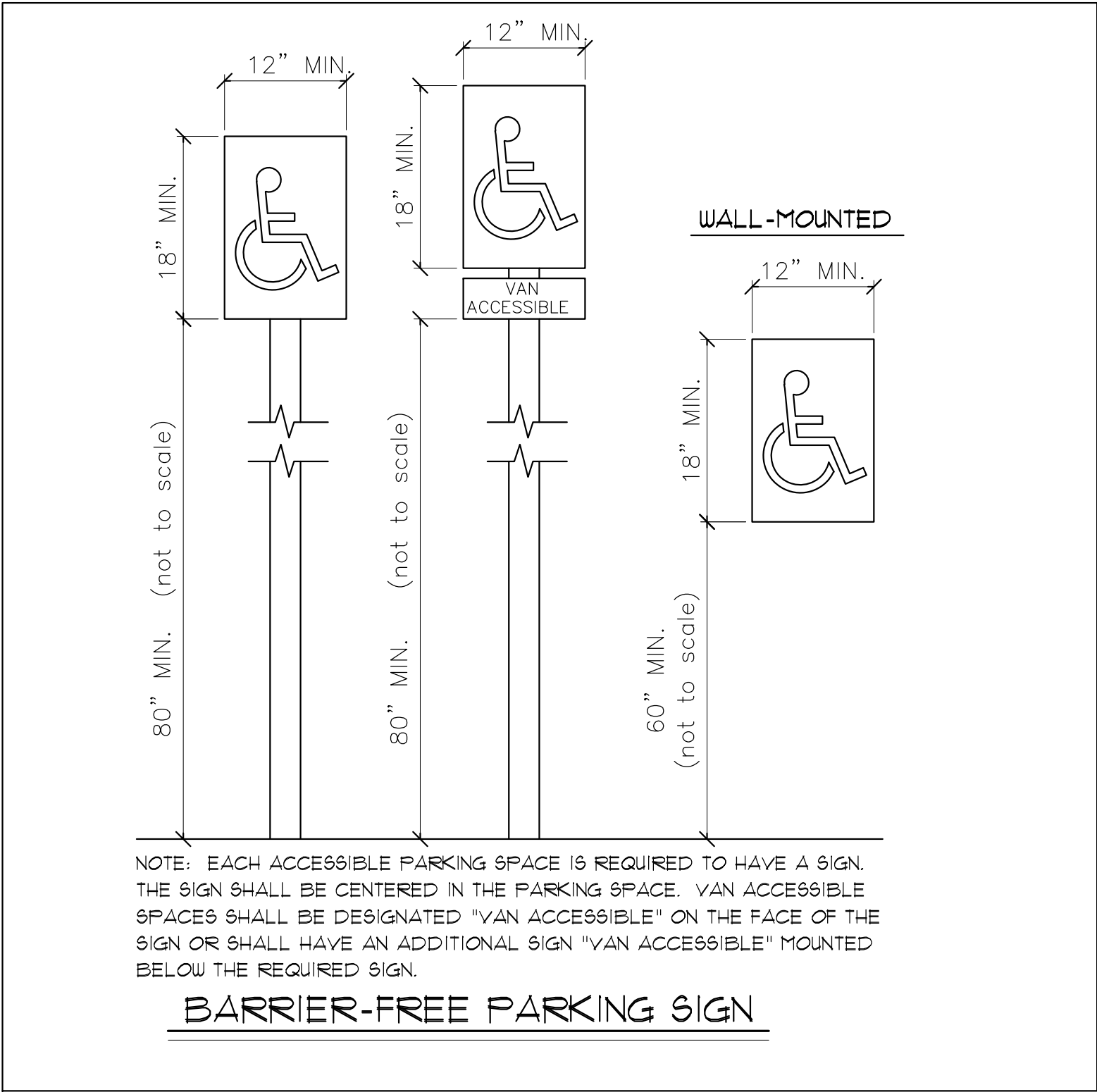
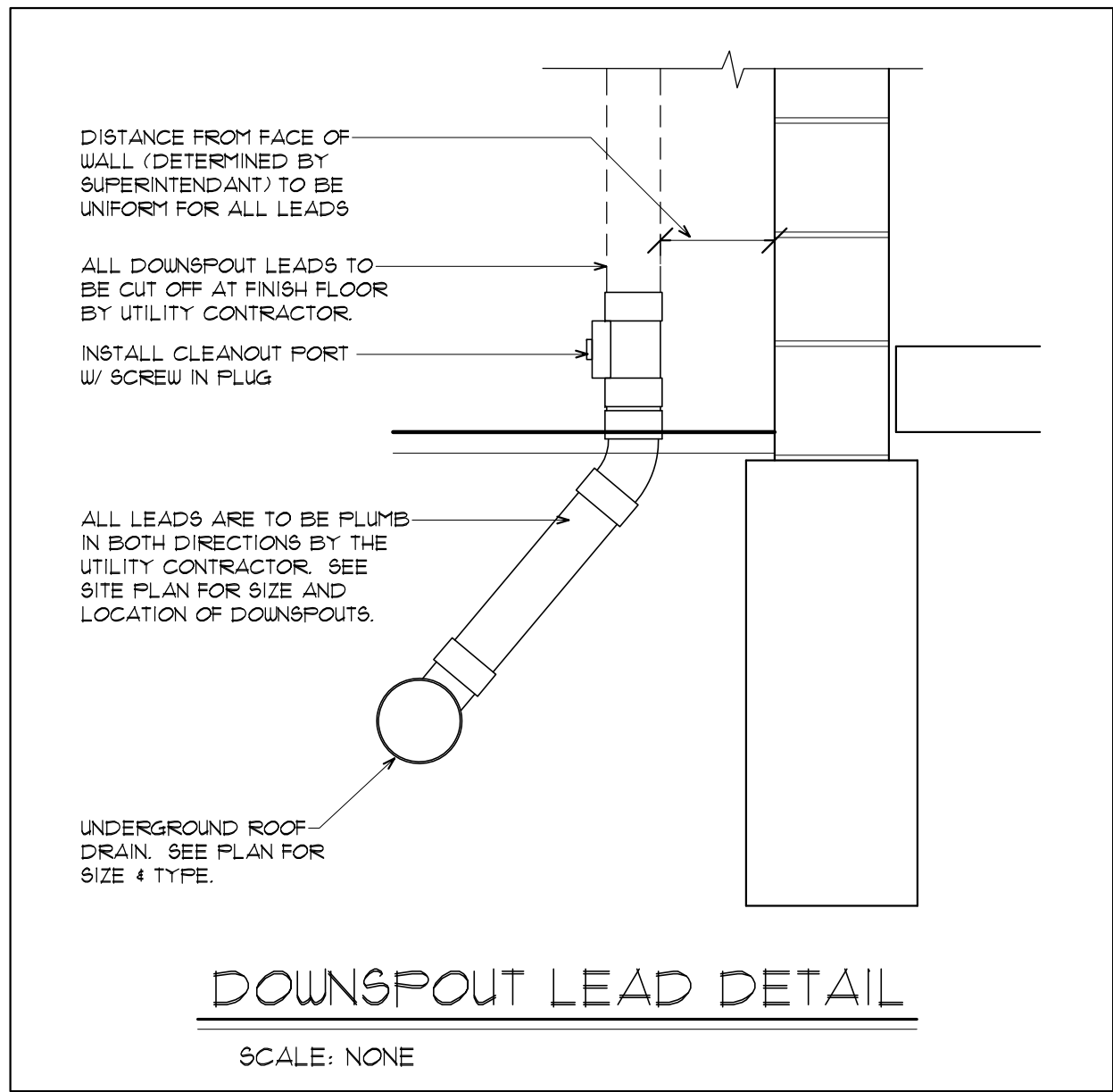
DRAWN BY: GAH  
JOB NO.: ---

LANDSCAPE PLAN  
SHEET NO.

C-4



MASONRY DUMPSTER DETAIL  
NO SCALE



| WASHTENAW COUNTY<br>PROPOSED DRAINAGE CALCULATION      | ACRES | ON-SITE |             |
|--------------------------------------------------------|-------|---------|-------------|
| Impervious Area (0.95)                                 | 0.44  | C=      | 0.61        |
| Pervious Area (0.30)                                   | 0.70  | A=      | 1.33 ACRES  |
| Impervious Area (0.85)                                 | 0.07  |         |             |
| Bankfull Basin (1.0)                                   | 0.13  |         |             |
| ALLOWABLE RELEASE RATE=                                |       |         | 0.15 CFS/AC |
| Q <sub>0(on-site)</sub> = ALLOWABLE RELEASE RATE x A = |       |         | 0.20 CFS    |

FIRST FLUSH VOLUME  
V<sub>ff</sub> = (1") (1/12") (43560 SF/1ac) x A x C = V<sub>ff</sub> = 2945 cf

|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                                                                                                                                                                                                                                                                                            |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>Pre-Development Bankfull Volume</b><br>2-year/24 hour storm event<br>Pre-Development CN<br>S = 1000/CN - 10 =<br>Q = (P-0.2S)/2 / (P+0.8S)<br>Total Site Area (sf) excl. S-C BMPs<br>V <sub>bf-pre</sub> = Q/12 x A<br><b>Pervious Cover Post-Development Bankfull Volume</b><br>2-year/24 hour storm event<br>Pervious Cover CN<br>S = 1000/CN - 10 =<br>Q = (P-0.2S)/2 / (P+0.8S)<br>Pervious Cover Area (sf)<br>V <sub>bf-per post</sub> = Q/12 x A <sub>p</sub><br><b>Impervious Cover Post-Development Bankfull Volume</b><br>2-year/24 hour storm event<br>Impervious Cover CN<br>S = 1000/CN - 10 =<br>Q = (P-0.2S)/2 / (P+0.8S)<br>Impervious Cover Area (sf)<br>V <sub>bf-imp post</sub> = Q/12 x A <sub>i</sub><br><b>Pervious Cover Post-Development 100-Year Volume</b><br>100-year storm event<br>Pervious Cover CN<br>S = 1000/CN - 10 =<br>Q <sub>100-per</sub> = (P-0.2S)/2 / (P+0.8S)<br>Pervious Cover Area (sf)<br>V <sub>100-per post</sub> = Q/12 x A <sub>p</sub><br><b>Impervious Cover Post-Development 100-Year Volume</b><br>100-year storm event<br>Impervious Cover CN<br>S = 1000/CN - 10 =<br>Q <sub>100-imp</sub> = (P-0.2S)/2 / (P+0.8S)<br>Impervious Cover Area (sf)<br>V <sub>100-imp</sub> = Q/12 x A <sub>i</sub> | <b>P=</b><br><b>CN=</b><br><b>S=</b><br><b>Q=</b><br><b>A=</b><br><b>V<sub>bf-pre</sub>=</b><br><b>P=</b><br><b>CN=</b><br><b>S=</b><br><b>Q=</b><br><b>A<sub>p</sub>=</b><br><b>V<sub>bf-per post</sub>=</b><br><b>P=</b><br><b>CN=</b><br><b>S=</b><br><b>Q=</b><br><b>A<sub>i</sub>=</b><br><b>V<sub>bf-imp post</sub>=</b><br><b>P=</b><br><b>CN=</b><br><b>S=</b><br><b>Q=</b><br><b>A<sub>100-per</sub>=</b><br><b>V<sub>100-per post</sub>=</b><br><b>P=</b><br><b>CN=</b><br><b>S=</b><br><b>Q=</b><br><b>A<sub>100-imp</sub>=</b><br><b>V<sub>100-imp</sub>=</b> | 2.35 in.<br>58<br>7.241 in.<br>0.100 in.<br>58060 sf<br>483 cf<br>2.35 in.<br>61<br>6.393 in.<br>0.154 in.<br>30455 sf<br>390 cf<br>2.35 in.<br>97<br>0.349 in.<br>1.978 in.<br>27605 sf<br>4550 cf<br>5.11 in.<br>61<br>6.393 in.<br>1.436 in.<br>30455 sf<br>3644 cf<br>5.11 in.<br>97<br>0.349 in.<br>4.714 in.<br>27605 sf<br>10844 cf |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|

|                                                                                                                                                                                                                                                         |                                                                                              |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|
| <b>Runoff Summary</b><br>V <sub>ff</sub> =<br>V <sub>bf-pre</sub> =<br>V <sub>bf-per post</sub> =<br>V <sub>bf-imp post</sub> =<br>V <sub>bf-post</sub> =<br>V <sub>p</sub> =<br>V <sub>100-per</sub> =<br>V <sub>100-imp</sub> =<br>V <sub>100</sub> = | 2945 cf<br>483 cf<br>390 cf<br>4550 cf<br>4940 cf<br>0 cf<br>3644 cf<br>10844 cf<br>14488 cf |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|

**On-Site Infiltration Requirement**  
Greater of First Flush volume or Difference between pre and post development bankfull volumes  
Bankfull Volume Difference = V<sub>bf-post</sub> - V<sub>bf-pre</sub> = 4457 cf

|                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                                                                                                                             |                                                                                               |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------|
| <b>INFILTRATION DESIGN</b><br>Required Infiltration<br>Depth of basin storage<br>Field Infiltration Rate<br>Design Infiltration Rate i <sub>d</sub> = i <sub>f</sub> / 2<br>Infiltration period<br>Infiltration Interface Area<br>Initial Infiltration Volume<br>V <sub>i</sub> = A <sub>i</sub> x i <sub>d</sub> (in/hr) x 1 (ft) (12 in) x t <sub>i</sub> (hr) =<br>Basin Storage Volume<br>Total Proposed Infiltration | V <sub>req-inf</sub> =<br>d =<br>i <sub>f</sub> =<br>i <sub>d</sub> =<br>t <sub>i</sub> =<br>A <sub>i</sub> =<br>V <sub>i</sub> =<br>V <sub>s</sub> =<br>V <sub>inf</sub> = | 4457 cf<br>1 ft<br>0.5 in/hr<br>0.25 in/hr<br>6 hr<br>4100 sf<br>512 cf<br>4100 cf<br>4612 cf |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------|

**On-Site Infiltration Proposed**  
On-Site design soil infiltration rate i<sub>d</sub> =  
**PROPOSED INFILTRAION V<sub>inf</sub>** =  
**INFILTRATION PERIOD T<sub>i</sub>** =

|                                  |
|----------------------------------|
| 0.25 in/hr<br>4612 cf<br>64.0 hr |
|----------------------------------|

| DRAINAGE AREA CALCULATIONS |            |           |          |          |             |    |      |
|----------------------------|------------|-----------|----------|----------|-------------|----|------|
| Pre-Development            | Cover Type | Soil Type | AREA(sf) | AREA(ac) | C Value     | CN | CN'A |
| B&B                        | Meadow     | B         | 58060    | 1.333    | 0.30        | 58 | 77   |
|                            |            | TOTAL     | 58060    | 1.333    | Weighted CN | 58 |      |
| Post-Development           | Cover Type | Soil Type | AREA(sf) | AREA(ac) | C Value     | CN | CN'A |
| Impervious                 | Pavement   | B         | 1165     | 0.027    | 0.95        | 98 | 3    |
|                            | Pond       | B         | 5500     | 0.126    | 1           | 98 | 12   |
|                            | Gravel     | B         | 2910     | 0.067    | 0.85        | 85 | 6    |
|                            | Building   | B         | 18000    | 0.413    | 0.95        | 98 | 40   |
|                            |            | TOTAL     | 27605    | 0.634    | Weighted CN | 97 |      |
| Pervious                   | Lawn       | B         | 30455    | 0.699    | 0.30        | 61 | 43   |
|                            |            | TOTAL     | 30455    | 0.699    | Weighted CN | 61 |      |

| Time of Concentration |      |              |            |             |                  |                        |                              |
|-----------------------|------|--------------|------------|-------------|------------------|------------------------|------------------------------|
| Flow Type             | K    | Elev. Change | Length (L) | Slope % (S) | S <sup>0.5</sup> | V=K * S <sup>0.5</sup> | T <sub>c</sub> =L / (V*3600) |
| Sheet Flow            | 0.48 | 4.0          | 300        | 1.300       | 1.140            | 0.547                  | 0.152                        |
| Waterway              | 1.20 | 0.5          | 100        | 1.300       | 1.140            | 1.368                  | 0.020                        |
| Small Tributary       | 2.10 | 0.0          | 0          | 0.000       | 0.000            | 0.000                  | 0.000                        |

|                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                                                                        |                                                                                                                  |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------|
| Q <sub>0</sub> = 238.6 x T <sub>c</sub> <sup>-0.82</sup> =<br>Total Site Area (ac) excl. SC-BMPs<br>Q <sub>100</sub> = Q <sub>100-per</sub> + Q <sub>100-imp</sub> =<br>Peak Flow (PF) = Q <sub>0</sub> x Q <sub>100</sub> x A / 640<br>Δ = PF(cfs) - 0.15(cfs/ac)*A(ac)<br>V <sub>0</sub> = Δ / PF x V <sub>100</sub><br>REQUIRED DETENTION VOLUME WITH INFILTRATION<br>V <sub>det</sub> = V <sub>0</sub> - V <sub>inf</sub> = | Q <sub>0</sub> =<br>A =<br>Q <sub>100</sub> =<br>PF =<br>Δ =<br>V <sub>0</sub> =<br>V <sub>det</sub> = | 0.17 hr<br>1007.77 cfs/in-mi <sup>2</sup><br>1.33 ac<br>6.15 in<br>12.91 cfs<br>12.71 cfs<br>14263 cf<br>9651 cf |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------|

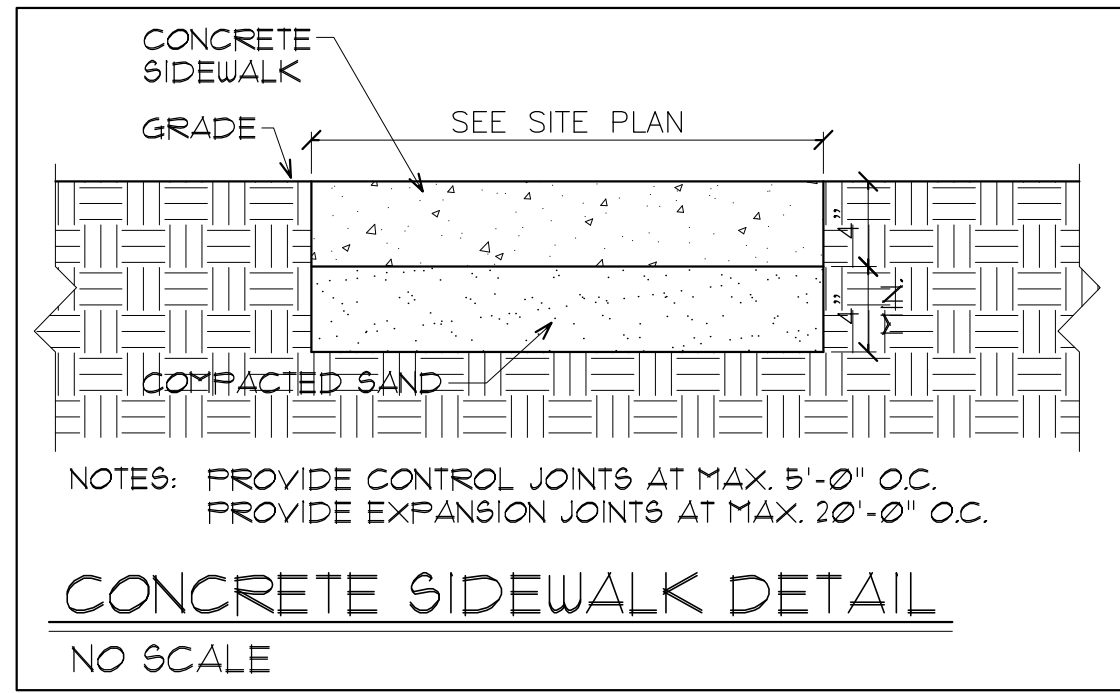
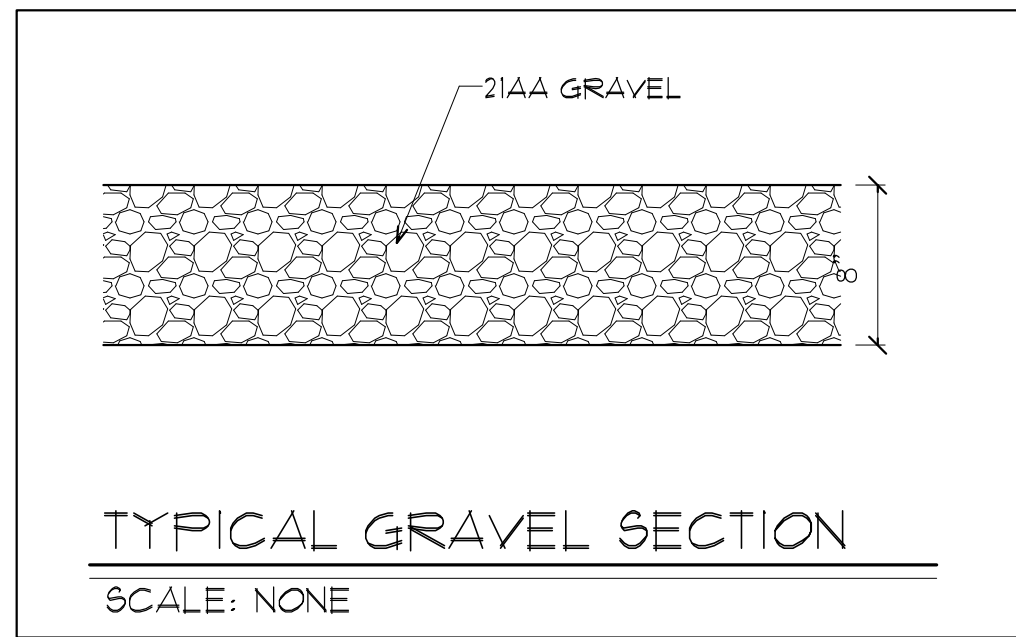
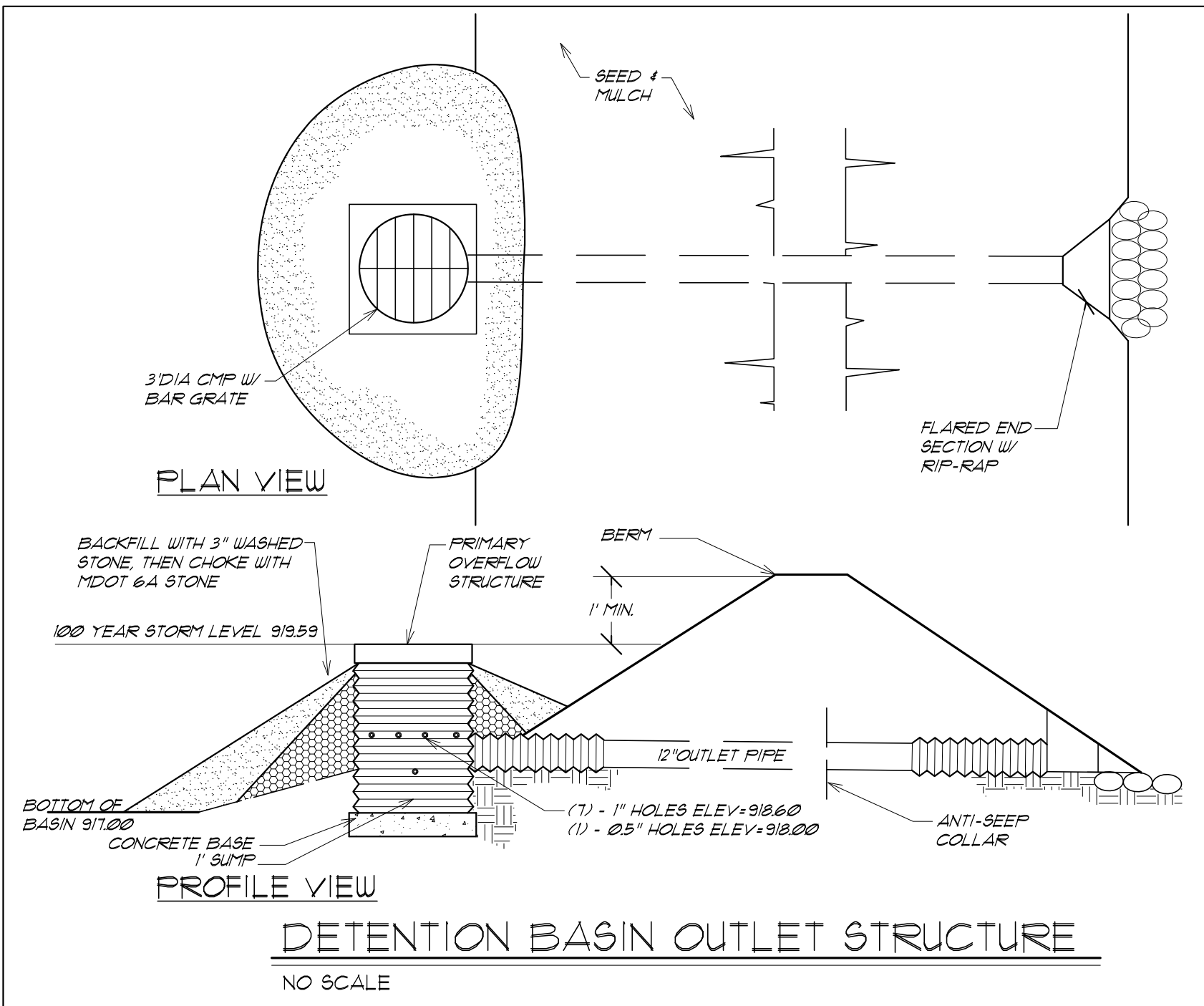
| BASIN STORAGE PROVIDED |                    |       |                    |                           |               |
|------------------------|--------------------|-------|--------------------|---------------------------|---------------|
| ELEV.                  | AREA               | DEPTH | VOLUME             | TOTAL                     |               |
|                        | (FT <sup>2</sup> ) | (FT)  | (FT <sup>3</sup> ) | VOLUME (FT <sup>3</sup> ) | Freeboard     |
| 920.6                  | 8935               | 0.6   | 5,041              | 17,592                    | Design Volume |
| 920                    | 7867               | 1     | 7,054              | 12,552                    |               |
| 919                    | 6240               | 1     | 5,498              | 5,498                     |               |
| 918                    | 4756               | 1     | 4,100              | 4,100                     | Infiltration  |
| 917                    | 3443               | 0     | 0                  | 0                         |               |

|                                                                        |                                                                                       |                                                |
|------------------------------------------------------------------------|---------------------------------------------------------------------------------------|------------------------------------------------|
| BOTTOM OF BASIN<br>INFILTRATION<br>FIRST FLUSH<br>BANKFULL<br>100 YEAR | X <sub>0</sub> =<br>X =<br>X <sub>FF</sub> =<br>X <sub>BF</sub> =<br>X <sub>0</sub> = | 917.00<br>918.00<br>917.72<br>918.60<br>919.59 |
|------------------------------------------------------------------------|---------------------------------------------------------------------------------------|------------------------------------------------|

**PROPOSED OUTLET CONTROL**  
**BANKFULL FLOOD**  
A PORTION OF THE BANKFULL VOLUME SHALL BE STORED FOR INFILTRATION  
THE REMAINING VOLUME SHALL DISCHARGE THROUGH HOLES AT THE TOP OF THE INFILTRATION STORAGE X  
REMAINING VOLUME = 328 CF  
Q<sub>BF</sub> = REMAINING VOLUME x (1 / 24HRS) x (1 / 3600SEC) = 0.004 CFS  
PLACE OPENINGS AT INFILTRATION STORAGE ELEVATION = 918.00  
h<sub>ave</sub> = 2/3 x (X<sub>BF</sub> - X<sub>0</sub>) = 0.40 FT  
A = Q<sub>BF</sub> / { (0.62 \* SQRT(2\*32.2\*h<sub>ave</sub>)) } = 0.001 SF  
A / 0.001 = 0.88  
THEREFORE, USE 1 INCH DIAMETER ORIFICE HAS AN AREA OF 0.001 SF  
1 0.5 INCH DIAMETER HOLES AT ELEV. = 918.00

**100 YEAR FLOOD**  
Q<sub>0</sub> = ALLOWABLE RELEASE RATE x AREA SITE IN ACRES = 0.20 CFS  
Q<sub>0</sub> IS A PEAK OR MAXIMUM FLOW. CALCULATE THE MAXIMUM FLOW PASSING THROUGH  
BANKFULL ORIFICES. USING THE TOTAL HEAD, AND SUBTRACT FROM Q<sub>0</sub> TO DETERMINE  
THE ORIFICE SIZE TO RELEASE THE 100 YEAR STORM VOLUME:  
Q<sub>BF</sub> = 0.62x#HOLESxPxAAREA EACH HOLExPxA(2\*32.2\*(X<sub>100</sub>-X<sub>0</sub>))<sup>0.5</sup>  
Q<sub>BF</sub> = 0.01 CFS  
Q<sub>0</sub> - (Q<sub>BF</sub>) = 0.19 CFS  
A = Q<sub>0</sub> / (0.62 \* (2 \* 32.2 \* (X<sub>100</sub>-X<sub>0</sub>))<sup>0.5</sup>) = 0.039 SF  
A / 0.005 = 7.10  
THEREFORE, USE THE FOLLOWING NUMBER OF 1" DIAMETER HOLES:  
7 HOLES AT ELEV. = 918.00

| SUMMARY OF REQUIRED STANDPIPE HOLES: |            |                   |
|--------------------------------------|------------|-------------------|
| ELEVATION                            | # OF HOLES | DIAMETER OF HOLES |
| 918.60                               | 7          | 1 in.             |
| 918.00                               | 1          | 0.5 in.           |



ANN ARBOR DOG TRAINING  
1575 E. North Territorial Road  
Northfield Township, Michigan

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ISSUED FOR: DATE:  
CONDITIONAL USE 3-9-17  
SITE PLAN 5-9-17  
REVISED 6-5-17

DRAWN BY: GAH/CLN  
JOB NO.:

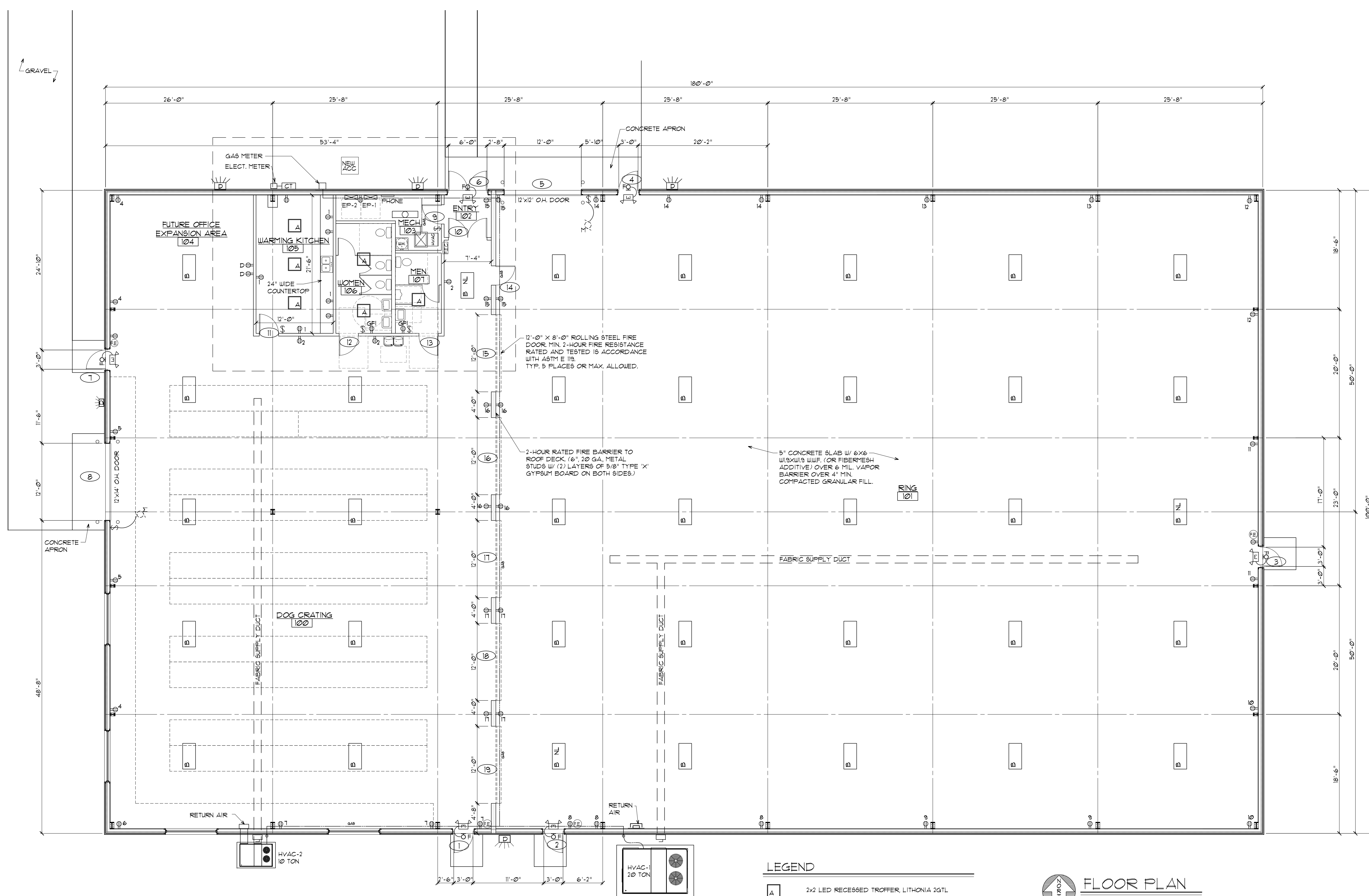
DETAIL SHEET  
SHEET NO.

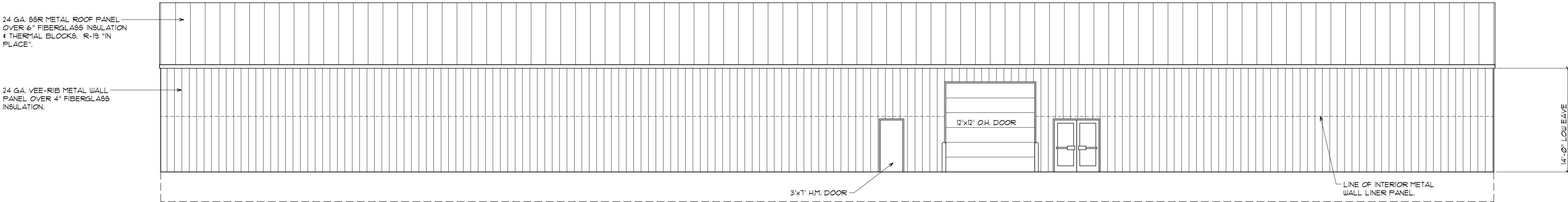
C-5

ANN ARBOR DOG TRAINING  
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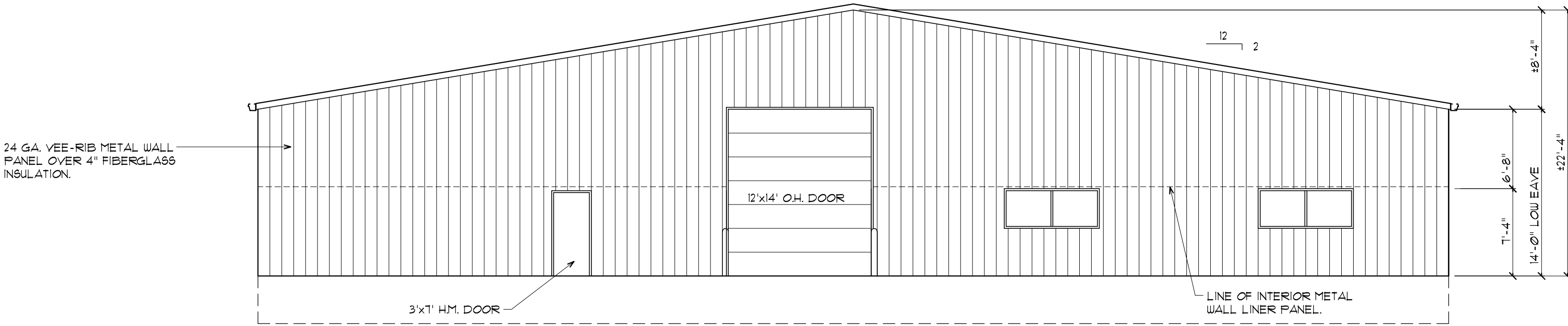
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| ISSUED FOR: | DATE:   |
|-------------|---------|
| REVIEW      | 5-31-12 |
| PROPOSAL    | 6-5-12  |
| REVISED     | 4-26-16 |
| REVISED     | 5-3-16  |
| PROPOSAL    | 7-11-16 |
| REVISED     | 5-17-17 |

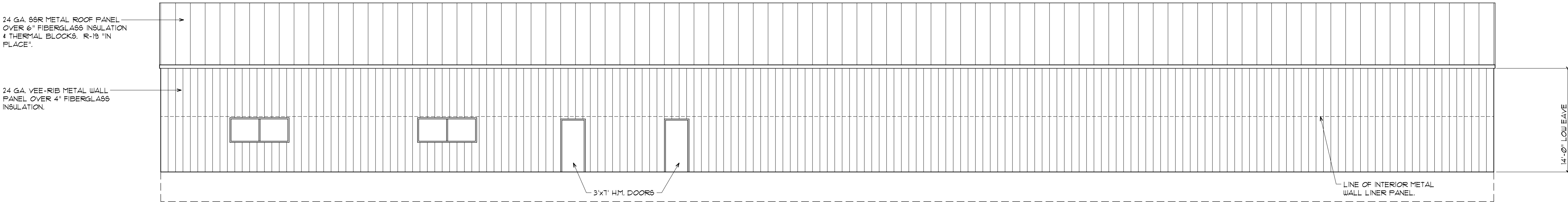
DRAWN BY: CLN/SA  
JOB NO.: -FLOOR PLAN  
SHEET NO.**A-1**



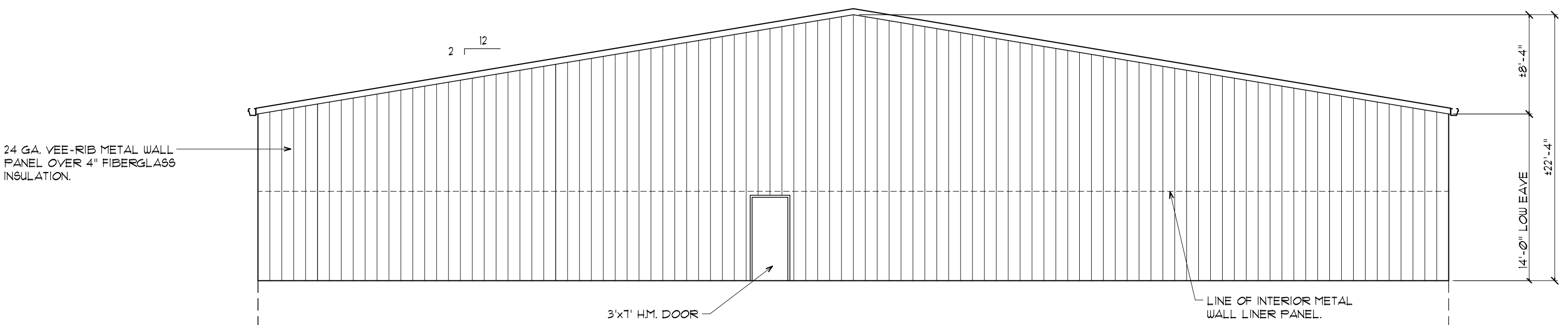
**NORTH ELEVATION**  
SCALE: 1/8" = 1'-0"



**WEST ELEVATION**  
SCALE: 1/8" = 1'-0"



**SOUTH ELEVATION**  
SCALE: 1/8" = 1'-0"



**EAST ELEVATION**  
SCALE: 1/8" = 1'-0"

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| REVISED     | 5-3-16  |
| PROPOSAL    | 7-11-16 |
| REVISED     | 5-17-17 |

DRAWN BY:

CLN

JOB NO.:

-

ELEVATIONS

SHEET NO.

**A-2**

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